

UNCLASSIFIED

AD NUMBER

AD837414

LIMITATION CHANGES

TO:

Approved for public release; distribution is unlimited.

FROM:

Distribution authorized to U.S. Gov't. agencies and their contractors; Critical Technology; JUL 1968. Other requests shall be referred to Army Electronics Command, AMSEL-KL-TD, Fort Monmouth, NJ. This document contains export-controlled technical data.

AUTHORITY

usaec ltr, 16 jun 1971

THIS PAGE IS UNCLASSIFIED

AD837414



Technical Report ECOM-01698-10

LONG-LIFE COLD CATHODE STUDIES FOR CROSSED-FIELD TUBES

PROGRESS REPORT

by

L. Lesensky - M. Arnum

C. McGeoch

JULY 1968

ECOM

UNITED STATES ARMY ELECTRONICS COMMAND - FORT MONMOUTH, N.J.

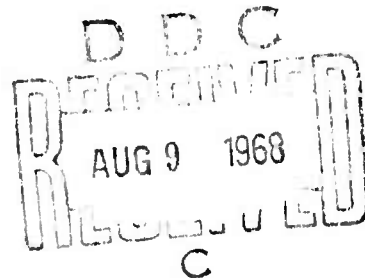
Contract DA28-043-AMC-01698 (E)

SPONSORED BY: ADVANCED RESEARCH PROJECTS AGENCY
ARPA ORDER NO. 345

RAYTHEON COMPANY
MICROWAVE AND POWER TUBE DIVISION
Waltham, Massachusetts

DISTRIBUTION STATEMENT

This document is subject to special export controls and each transmittal to foreign governments or foreign nationals may be made only with prior approval of CG, U.S. Army Electronics Command, Fort Monmouth, New Jersey.
Attn: AMSEL-KL-TD



**BEST
AVAILABLE COPY**

Technical Report ECOM-01698-10

Reports Control Symbol
OSD-1366
July 1968

LONG-LIFE COLD CATHODE STUDIES
FOR CROSSED-FIELD TUBES

Tenth Quarterly Report
15 January 1968 to 15 April 1968

Report No. 10
Contract No. DA28-043-AMC-01698(E)
DA Project No. 7900-21-223-12-00

Prepared by
L. Lesensky
M. Arnum
C. McGeoch

RAYTHEON COMPANY
Microwave and Power Tube Division
Waltham, Massachusetts 02154

For
U.S. Army Electronics Command
Fort Monmouth, N. J. 07703

Sponsored by
Advanced Research Projects Agency
ARPA Order No. 345

DISTRIBUTION STATEMENT

This document is subject to special export controls and each transmittal to foreign governments or foreign nationals may be made only with prior approval of CG, U.S. Army Electronics Command, Fort Monmouth, New Jersey.
Attn: AMSEL-KL-TD

ABSTRACT

Further tests of the effects of high current-density electron bombardment (0.75 A/cm^2) and of residual oxygen ($\sim 1.5 \times 10^{-5} \text{ Torr}$) on the secondary emission ratio (δ) were performed in the Electron Bombardment Vehicle (EBV). δ_{max} for a 300Å electron-beam-evaporated layer of alumina on molybdenum increased from 2.0 to 3.8 due to O_2 pressure of $1.5 \times 10^{-5} \text{ Torr}$, and decreased from 3.8 to 2.0 due to 0.75 A/cm^2 electron bombardment without oxygen. δ_{max} for an anodized beryllium target (300Å oxide layer) increased from 1.9 to 3.0 under the same O_2 treatment.

Operation of the QKS1397 CFA test vehicle for more than 200 hours has shown that the available emission (using the O_2 dispenser) from an evaporated aluminum-on-copper cold cathode appears to have stabilized near a peak current of 40 amperes ($\sim 2 \text{ A/cm}^2$) at a 0.002 duty factor. Approximately 70 hours of operation were obtained at 2.5 A/cm^2 .

FOREWORD

Long-life cold cathode studies for crossed-field tubes are authorized by the United States Army Electronics Command, Fort Monmouth, New Jersey, under DA Project No. 7900-21-223-12-00. The work was prepared under the support of the Advanced Research Projects Agency under Order No. 345 and is conducted under the technical guidance of the U. S. Army Electronics Command, Fort Monmouth, N. J. 07703.

TABLE OF CONTENTS

| <u>Section</u> | | <u>Page</u> |
|----------------|---|-------------|
| 1. | Introduction | 1 |
| 2. | Phase A - Materials Evaluation | 1 |
| 2.1 | Electron Bombardment Evaluation | 1 |
| 2.1.1 | 300Å Electron-Beam-Evaporated Alumina on Molybdenum | 2 |
| 2.1.2 | Anodized Beryllium - 300Å Oxide Layer | 2 |
| 2.1.3 | Anodized Aluminum (Alloy 1100) - 300Å Oxide Layer | 2 |
| 2.1.4 | Nickel-Cermet Sample in Hot/Cold EBV | 2 |
| 3. | Phase B - CFA Testing | 2 |
| 3.1 | QKS1397 Test Vehicle | 2 |
| 3.1.1 | Model No. 8C | 2 |
| 4. | Conclusions | 7 |
| 4.1 | Phase A - Materials Evaluation | 7 |
| 4.2 | Phase B - CFA Testing | 7 |
| 5. | Program for Next Interval | 8 |
| 5.1 | Phase A | 8 |
| 5.2 | Phase B | 8 |

LIST OF ILLUSTRATIONS

| <u>Figure No.</u> | <u>Title</u> | <u>Page</u> |
|-------------------|--|-------------|
| 1. | δ_{\max} vs EBV Time for 300Å Al_2O_3 on Molybdenum | 3 |
| 2. | δ_{\max} vs EBV Time for 300Å Anodized Beryllium | 4 |
| 3. Sheet 1 | QKS1397 No. 8C - $p_{\text{in}}=110$ kW, $B=3000$ gauss | 6 |
| 3. Sheet 2 | QKS1397 No. 8C - $p_{\text{in}}=110$ kW, $B=3000$ gauss | 7 |

1. INTRODUCTION

The objective of the present cold cathode study program is to achieve long life cold-cathode performance for crossed-field amplifiers. This program is being performed for the United States Army Electronics Command, Fort Monmouth, New Jersey, under contract DA-28-043-AMC-01698(E).

In this study, selected cold cathode materials will be evaluated as to their secondary emission properties, their ability to withstand environmental factors expected in a crossed-field amplifier, and their crossed-field amplifier performance. Based on the above experimental information and pertinent theoretical calculations, a life prediction chart will be established for a number of cold cathode materials.

The program is divided into two concurrent phases, Phase A being concerned with the measurement of various pertinent properties of cold cathode materials outside of the tube environment, and Phase P involving the evaluation and life testing of selected cathodes in a crossed-field amplifier.

The first quarterly report of this contract (Technical Report ECOM 01698-1) contains a discussion of the objectives and plans for the over-all program. Quarterly Report No. 5 contains a description of the CFA test vehicles used in this program.

2. PHASE A - MATERIALS EVALUATION

2.1 Electron Bombardment Evaluation. During the present quarter, several samples were evaluated in the Electron Bombardment Vehicle (EBV). The effort on secondary emission ratio (δ) of high current-density electron bombardment (up to 0.75 A/cm^2) was measured as well as recovery with oxygen. These samples were as follows:

- a. 300Å aluminum-oxide layer on 1100 aluminum (anodically oxidized) - 20 hour continuation of sample A-2.
- b. Another anodized 1100 Al sample (like A-2) - sample A3 for 30 hours.
- c. A nickel-cermet sample for 6 hours on the hot/cold EBV.
- d. 300Å electron-beam-evaporated layer of alumina on Mo for 41 hours.
- e. 300Å layer BeO on Be (anodically oxidized), 37 hours.

The following samples were prepared during the present quarter:

- a. Four 300Å electron-beam-evaporated alumina on Mo samples for EBV.
- b. Four Be samples for EBV. These were diffusion-bonded to copper. Two of these samples were anodically oxidized by the tartaric acid method to form a 300Å BeO layer on Be.

- c. Eight beryllium-copper samples for EBV were machined.
- d. Eight silver-magnesium samples for EBV were machined.

In addition several EBV gun units were assembled.

2.1.1 300Å Electron-Beam-Evaporated Alumina on Molybdenum.

During a 41-hour period of electron bombardment evaluation, δ_{\max} varied between 2.0 and 3.8 (Figure 1). In order to achieve 3.8 it was necessary to admit O_2 . While O_2 was admitted to a pressure of 1.5×10^{-5} Torr and during electron bombardment at 0.15 A/cm^2 (corresponding to 3 mA), δ_{\max} rose from 2.0 to 3.8. After the O_2 was pumped away, electron bombardment at 0.75 A/cm^2 (corresponding to 15 mA) caused δ_{\max} to decrease from 3.8 to 2.2 in nine hours. Testing of this sample is continuing.

2.1.2 Anodized Beryllium - 300Å Oxide Layer.

During a 37-hour period of electron bombardment evaluation, δ_{\max} varied between 1.6 and 3.0 (Figure 2). O_2 at 1.5×10^{-5} Torr caused a significant increase in δ_{\max} , particularly with 3 mA bombardment rather than with no bombardment. Perhaps some temperature increase is beneficial to surface reoxidation. After the O_2 was pumped away, δ_{\max} decreased due to electron bombardment, 0.75 A/cm^2 causing a more rapid decrease than 0.15 A/cm^2 .

2.1.3 Anodized Aluminum (Alloy 1100) - 300Å Oxide Layer.

Sample A-2, reported in the 9th Quarterly, was continued for 19 hours (hours 55 to 74) under 0.5 A/cm^2 electron bombardment without O_2 . During this period, δ_{\max} remained essentially constant at 2.3.

Another similar sample (A-3) was evaluated for a 30-hour period. δ_{\max} remained at 1.5 during the initial 15-hour period of electron bombardment without O_2 . Up to 0.75 A/cm^2 bombardment was employed. Then O_2 was admitted up to a pressure of 1.6×10^{-5} Torr. δ_{\max} rose slightly to a value of 2.0. Further testing of this sample was discontinued due to the lack of response to O_2 usually observed.

2.1.4 Nickel-Cermet Sample in Hot/Cold EBV.

Another nickel-cermet sample was installed in the Hot/Cold EBV. Thermal activation of the sample was attempted over a 5-hour period, during which it was at 900°C for two hours. The minimum value of δ_{\max} was 1.5 and the maximum value was 1.8. Apparently the activation was not successful. The test was terminated due to a leak in the gun housing. The gun unit has been replaced and further EBV evaluation of a nickel-cermet sample will be attempted in the next quarterly period.

3. PHASE B - CFA TESTING

3.1 QKS1397 Test Vehicle

3.1.1 Model No. 8C.

Cathode emission life-test evaluation was conducted on Model 8C during the report period, at a cathode-pulsed modulation test station. The cathode emitter consisted of 0.0005-inch aluminum deposited on an OFHC copper base. The cathode was 1.645 inches in diameter, 0.670 inch axial height for an emitter surface area of 22.4 sq. cm.

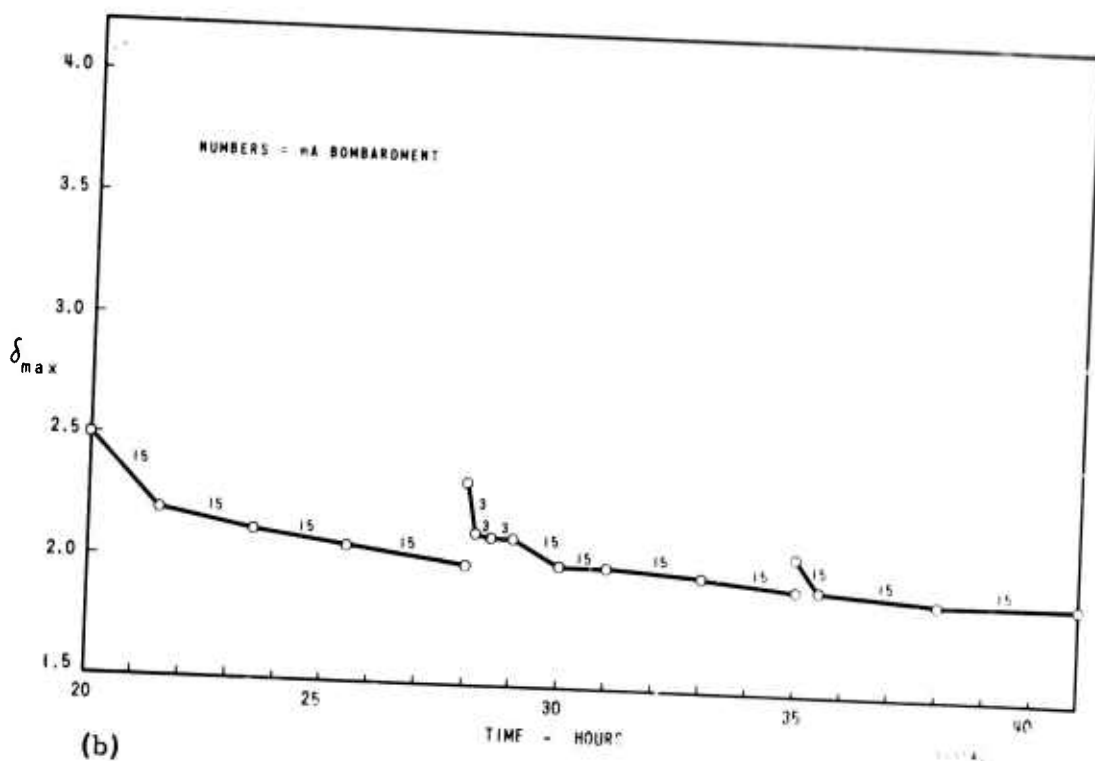
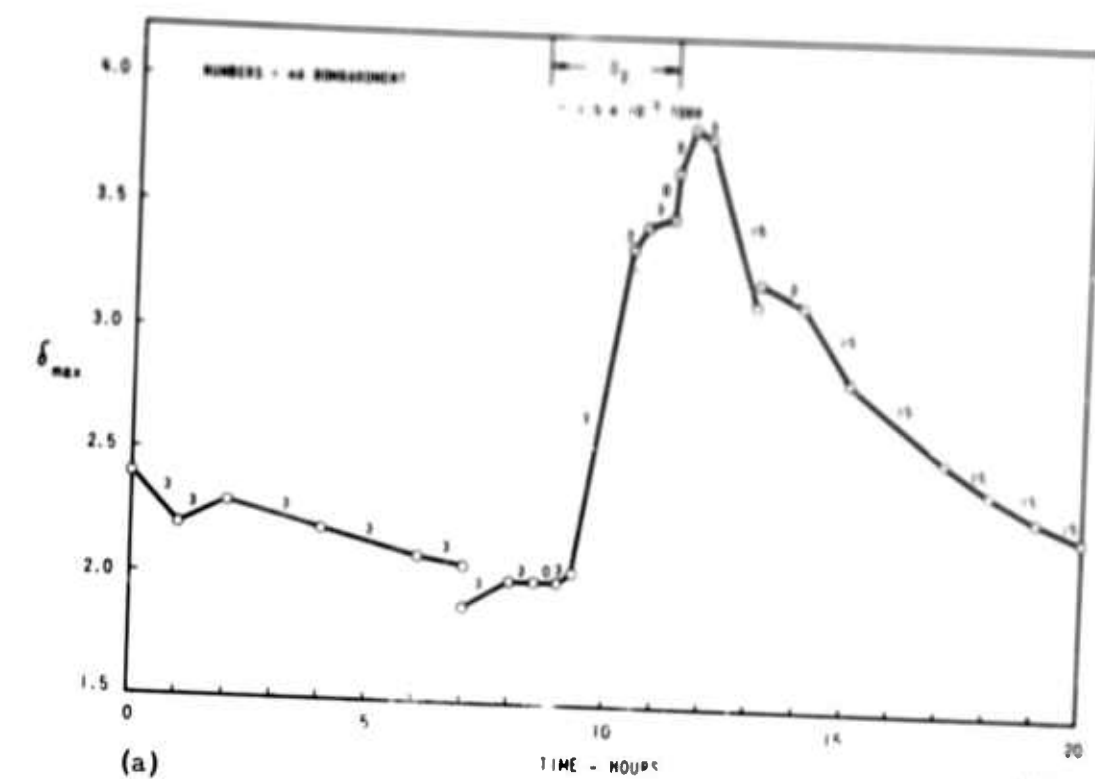


Figure 4 δ_{max} vs EBV Time for 300\AA Al_2O_3 on Molybdenum

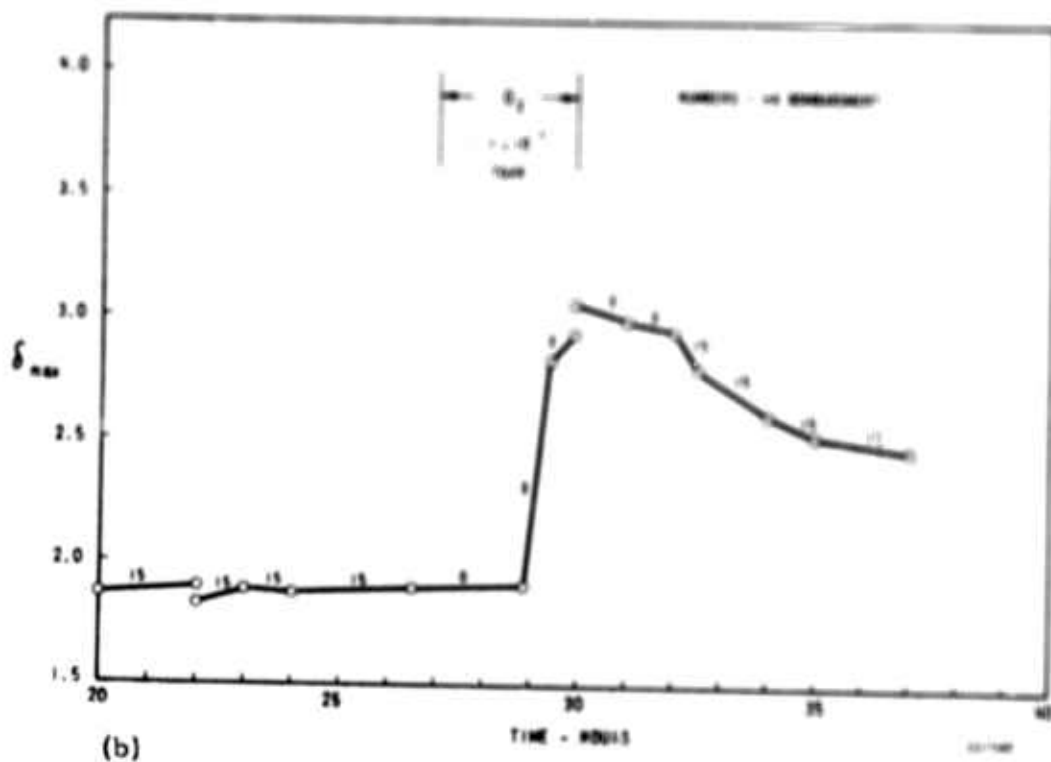
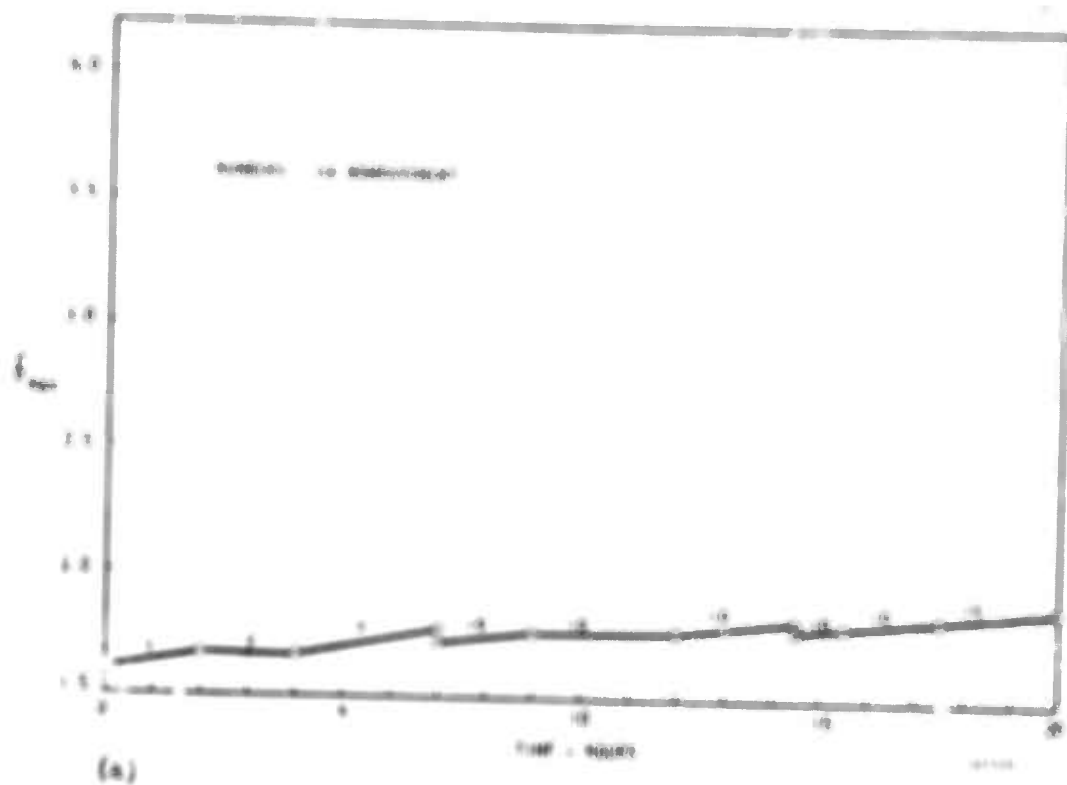


Figure 5 δ_{max} vs EBV Time for 300A Anodized Beryllium

In Figure 2, the solid line shows the peak current, and the dashed line the oxygen-displacement heater power, both as a function of time for the duration of the testing completed to date. The maximum current emission available is also indicated by I_p as a function of heater power at the 1.5 sec period.

Initially the operating peak current level was chosen at 54.5 ampere, at the following operating conditions:

$$\begin{aligned} Q_h &= 0.001 \\ f_c &= 1.5 \text{ GHz} \\ P_{in} &= 110 \text{ kW} \\ P_o &= 400 \text{ kW} \\ E_p &= 11 \text{ eV} \\ R &= 2000 \text{ gauss} \end{aligned}$$

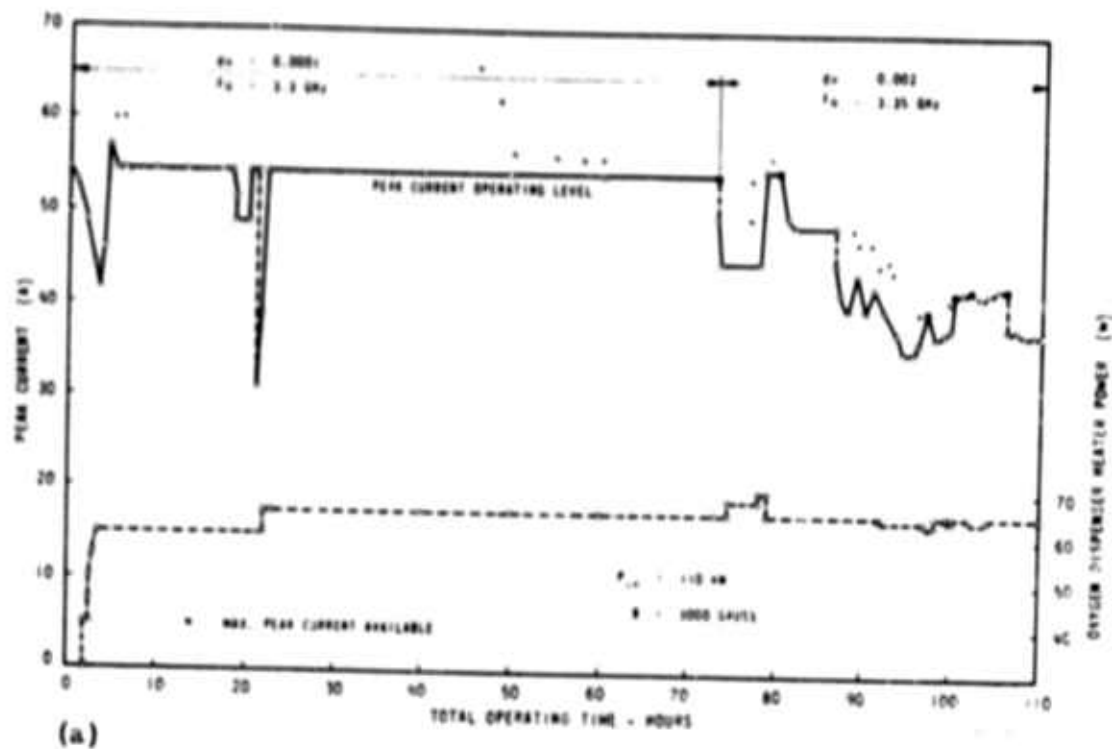
This level of emission could not be maintained without use of the oxygen dispenser. The oxygen-displacement heater power was therefore gradually increased to 40 watts, at which point the emission had recovered sufficiently for operation at the level initially selected.

In the period 18 - 22 hours of operating time, the drive-pulse trigger amplifier became unstable, which caused the tube to arc, with resultant loss of emission. After repairs and emission reconditioning by increasing the oxygen-displacement heater power to 57 watts, life testing was continued at the initially selected peak-current level through the 72nd hour of operation. At this point the maximum peak current available had decreased to the operating current level.

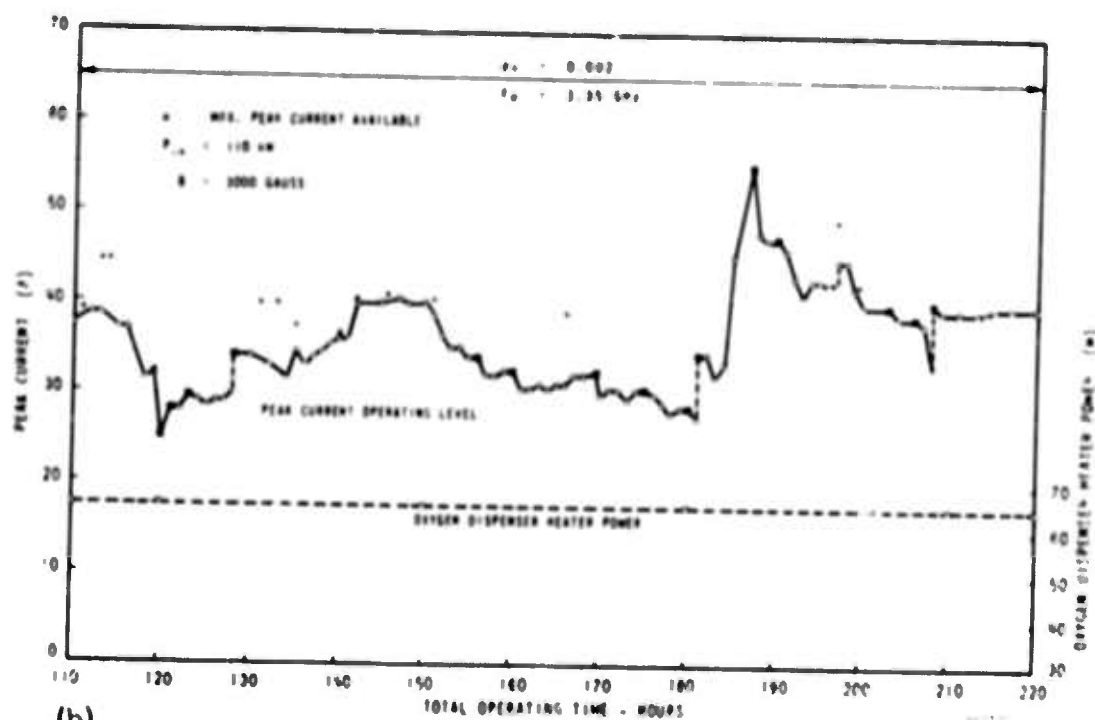
The operating conditions were now changed to a duty factor of 0.002 and a frequency of 1.35 GHz. An immediate decline in the peak current available was observed, although it could be recovered by increasing the oxygen-displacement heater power to 70 watts. However, operation at this heater-power level shortens the oxygen pellet life; the heater power was therefore restored within a short time to 57 watts.

After approximately 110 hours of operation, the test-vehicle trigger amplifier became erratic, which caused the tube to arc, with consequent loss of emission. The emission gradually recovered after repairing the trigger-amplifier unit. At 140 hours of operation, the emission was further increased by increasing the peak drive power to 125 kW. After about 10 hours of operation at this level, the drive power was restored to 110 kW, with the resultant continual decrease in peak-current emission.

At 162 hours of operating time the oxygen-displacement power supply leads were shortened by eliminating all clip leads. This apparently reduced the lead resistance, and thereby increased the power available for heating the oxygen-displacement pellet. The peak-current emission available showed an immediate increase to 76 peak ampere, but again could not be maintained. At the end of the report period (235 hours) the peak-current emission appeared to have settled near 40 ampere.



(a)



(b)

Figure 10 QKS1397 No. 8C - $p_{\text{in}} = 110 \text{ kW}$, $B = 3000 \text{ Gauss}$
0.0005 in. Evaporated Al on Cu Emitter

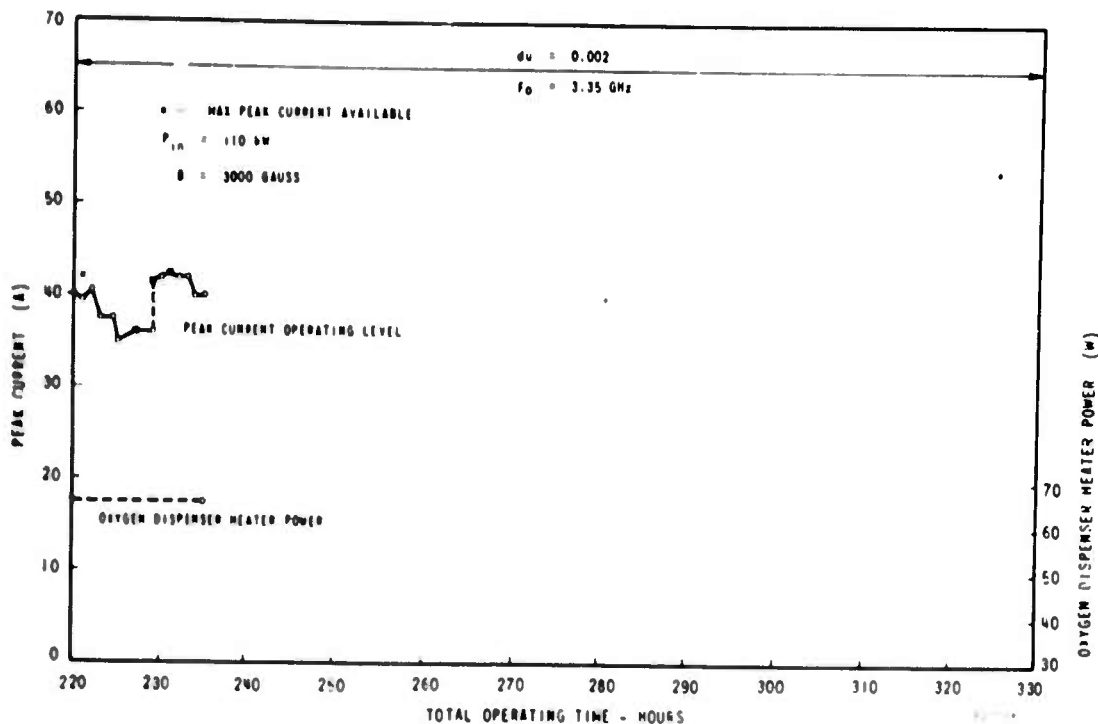


Figure 3 - Sheet 2. QKS1397 No. 8C - $p_{in} = 110 \text{ kW}$, $B = 3000 \text{ gauss}$

4. CONCLUSIONS

4.1 Phase A - Materials Evaluation.

- a. 300\AA oxide layers of electron-beam-evaporated alumina on molybdenum, anodized beryllium, and anodized aluminum, show generally similar behavior in terms of beneficial response to oxygen and deterioration of δ due to electron bombardment at 0.75 A/cm^2 .
- b. A possible interpretation of some of the data reported above is that some elevation of temperature above room temperature may be beneficial in the response of δ to O_2 for a beryllium or aluminum sample.

4.2 Phase B - CFA Testing. Operation of the QKS1397 CFA test vehicle for more than 200 hours has shown that the available emission from a deposited aluminum cold cathode appears to have stabilized near 40 amperes, at a 0.002 duty factor. At 0.001 duty factor, approximately 70 hours of operation was obtained at a peak current level of 54.5 amperes. Activation of the O_2 dispenser was required throughout the test period to maintain the cathode emission.

5. PROGRAM FOR NEXT INTERVAL

5.1 Phase A

- a. Continue testing of electron-beam-evaporated alumina on Mo sample.
- b. Continue testing of anodized beryllium sample.
- c. Test a new nickel-cermet sample.
- d. Process Ag-Mg and Be-Cu samples for EBV.
- e. Test the Ag-Mg and Be-Cu samples.

5.2 Phase B

- a. Continue life testing of QKS1397 model 8C.
- b. Rebuild the QKS1397 test vehicle with an impregnated tungsten cathode.
- c. Accumulate additional operating life on the impregnated cathode in the QKS1194 test vehicle.

DOCUMENT CONTROL DATA - R&D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author)

Raytheon Company
Microwave and Power Tube Division
Waltham, Massachusetts

2a. REPORT SECURITY CLASSIFICATION

Unclassified

2b. GROUP

N/A

3. REPORT TITLE

Long-Life Cold Cathode Studies for Crossed-Field Tubes

4. DESCRIPTIVE NOTES (Type of report and inclusive dates)

Tenth Quarterly Report 15 January 1968 - 15 April 1968

5. AUTHOR(S) (Last name, first name, initial)

Lesensky, L; Arnum, M; and McGeoch, C.

6. REPORT DATE

July 1968

7a. TOTAL NO. OF PAGES

8

7b. NO. OF REFS

0

8a. CONTRACT OR GRANT NO.

DA28-043-AMC-01698(E)

b. PROJECT NO.

7900-21-223-12-00

c.

d.

9a. ORIGINATOR'S REPORT NUMBER(S)

PT-1897

9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)

ECOM-01698-10

10. AVAILABILITY/LIMITATION NOTICES

This document is subject to special export controls and each transmittal to foreign governments or foreign nationals may be made only with prior approval of CG, USAECOM, ATTN: AMSEL-KL-TD, Fort Monmouth, N.J. 07703

11. SUPPLEMENTARY NOTES

Advanced Research Projects
Agency Contract ARPA Order
No. 345

12. SPONSORING MILITARY ACTIVITY

U. S. Army Electronics Command
Fort Monmouth, N.J. 07703
AMSEL-KL-TD

13. ABSTRACT

Further tests on the effects of high current-density electron bombardment (0.75 A/cm^2) and of residual oxygen ($\sim 1.5 \times 10^{-5} \text{ Torr}$) on the secondary emission ratio (δ) were performed in the Electron Bombardment Vehicle (EBV). δ_{max} for a 300\AA electron-beam-evaporated layer of alumina on molybdenum increased from 2.0 to 3.8 due to O_2 pressure of $1.5 \times 10^{-5} \text{ Torr}$, and decreased from 3.8 to 2.0 due to 0.75 A/cm^2 electron bombardment without oxygen. δ_{max} for an anodized beryllium target (300\AA oxide layer) increased from 1.9 to 3.0 under the same O_2 treatment.

Operation of the QKS1397 CFA test vehicle for more than 200 hours has shown that the available emission (using the O_2 dispenser) from an evaporated aluminum-on-copper cold cathode appears to have stabilized near a peak current of 40 amperes ($\sim 2 \text{ A/cm}^2$) at a 0.002 duty factor. Approximately 70 hours of operation were obtained at 2.5 A/cm^2 .

| 14. KEY WORDS | LINK A | | LINK B | | LINK C | |
|--|--------|----|--------|----|--------|----|
| | ROLE | WT | ROLE | WT | ROLE | WT |
| Secondary Emission Cold Cathode Crossed-Field Amplifiers Electron Bombardment Ion Bombardment Thin Films Aluminum Oxide Beryllium Oxide | | | | | | |

INSTRUCTIONS

1. **ORIGINATING ACTIVITY:** Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (*corporate author*) issuing the report.

2a. **REPORT SECURITY CLASSIFICATION:** Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

2b. **GROUP:** Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.

3. **REPORT TITLE:** Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.

4. **DESCRIPTIVE NOTES:** If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.

5. **AUTHOR(S):** Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.

6. **REPORT DATE:** Enter the date of the report as day, month, year; or month, year. If more than one date appears on the report, use date of publication.

7a. **TOTAL NUMBER OF PAGES:** The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.

7b. **NUMBER OF REFERENCES:** Enter the total number of references cited in the report.

8a. **CONTRACT OR GRANT NUMBER:** If appropriate, enter the applicable number of the contract or grant under which the report was written.

8b, 8c, & 8d. **PROJECT NUMBER:** Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

9a. **ORIGINATOR'S REPORT NUMBER(S):** Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

9b. **OTHER REPORT NUMBER(S):** If the report has been assigned any other report numbers (*either by the originator or by the sponsor*), also enter this number(s).

10. **AVAILABILITY/LIMITATION NOTICES:** Enter any limitations on further dissemination of the report, other than those

imposed by security classification, using standard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through _____."
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through _____."
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through _____."

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

11. **SUPPLEMENTARY NOTES:** Use for additional explanatory notes.

12. **SPONSORING MILITARY ACTIVITY:** Enter the name of the departmental project office or laboratory sponsoring (*paying for*) the research and development. Include address.

13. **ABSTRACT:** Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (C), or (U).

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

14. **KEY WORDS:** Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, rules, and weights is optional.